

Principles of Communications

Chapter 3: Analog Modulation
(continued)

Textbook: Ch 3, Ch 4.1-4.4

3.3 Angle Modulation

- Angle modulation is either **phase** or **frequency** of the carrier is varied according to the message signal
- The general form of an **angle modulated wave** is

$$s(t) = A_c \cos[2\pi f_c t + \theta(t)]$$

where f_c = carrier freq, $\theta(t)$ is the time-varying phase and varied by the message $m(t)$

- The **instantaneous frequency** of $s(t)$ is

$$f_i(t) = f_c + \frac{1}{2\pi} \frac{d\theta(t)}{dt}$$

Representation of FM and PM signals

- For phase modulation (PM), we have

$$\theta(t) = k_p m(t) \quad \text{where } k_p = \text{phase deviation constant}$$

- For frequency modulation (FM), we have

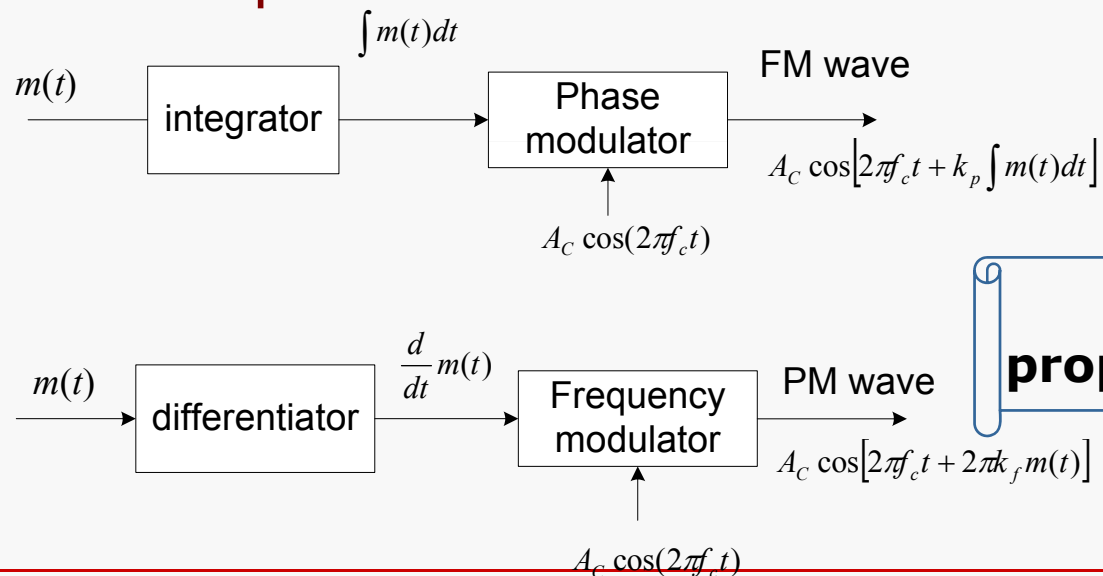
$$f_i(t) - f_c = k_f m(t) = \frac{1}{2\pi} \frac{d}{dt} \theta(t) \quad \text{where } k_f = \text{frequency deviation constant}$$

- The phase of FM is

$$\theta(t) = 2\pi k_f \int_0^t m(\tau) d\tau$$

Distinguishing Features of PM and FM

- ❑ No perfect regularity in spacing of **zero crossing**
 - Zero crossings refer to the **time instants** at which a **waveform changes between negative and positive values**
- ❑ Constant envelop, i.e. amplitude of $s(t)$ is constant
- ❑ **Relationship between PM and FM**



Discuss the properties of FM only

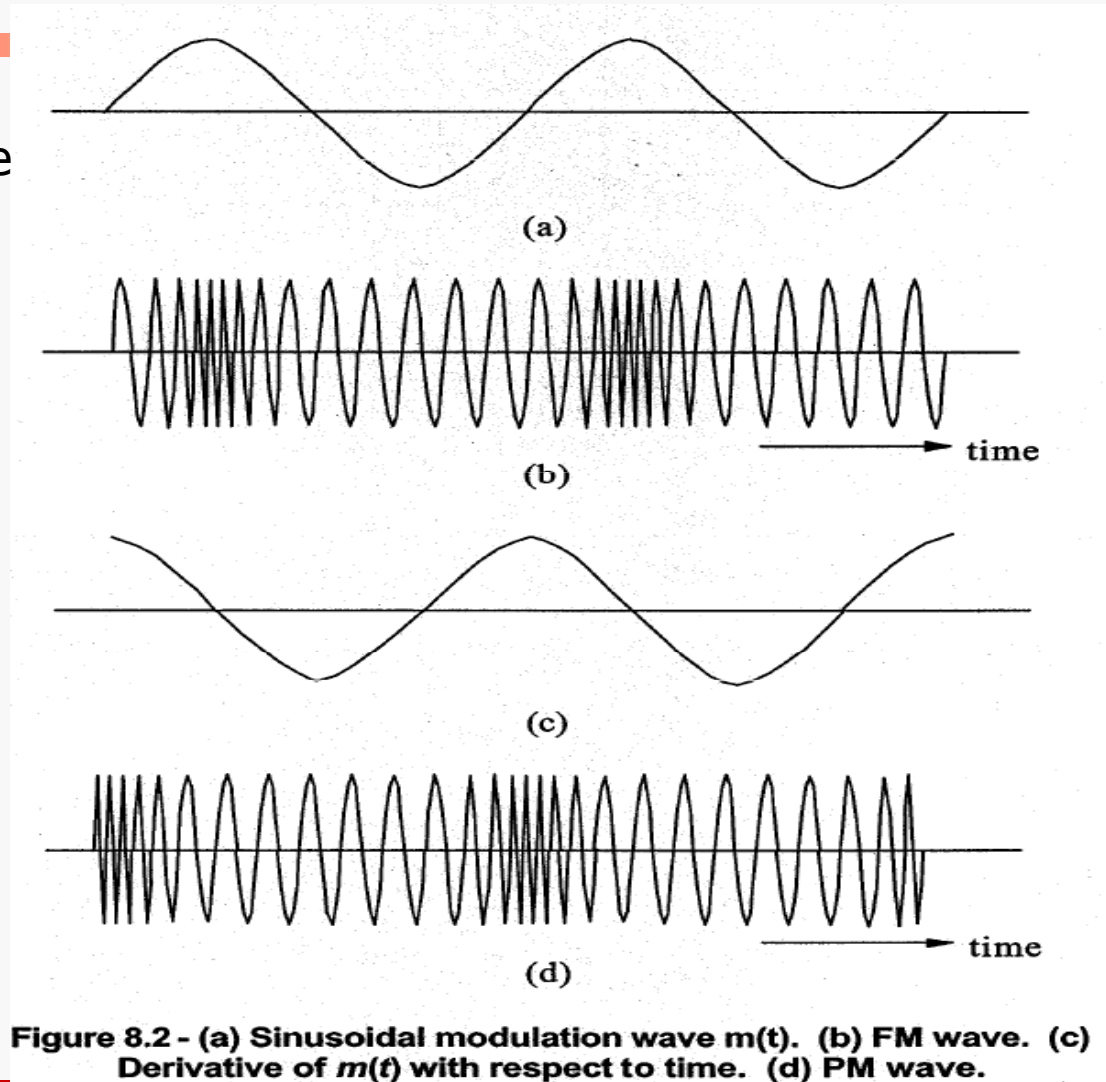
Example: Sinusoidal Modulation

Sinusoid
modulating wave
 $m(t)$

FM wave

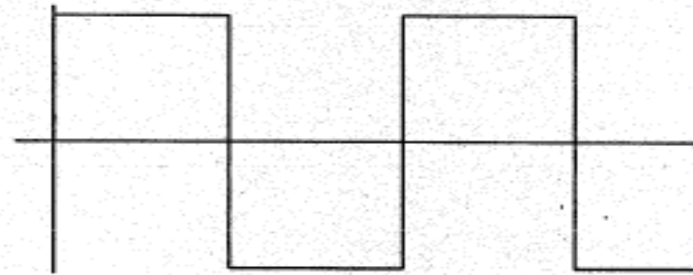
$$\frac{d}{dt}m(t)$$

PM wave



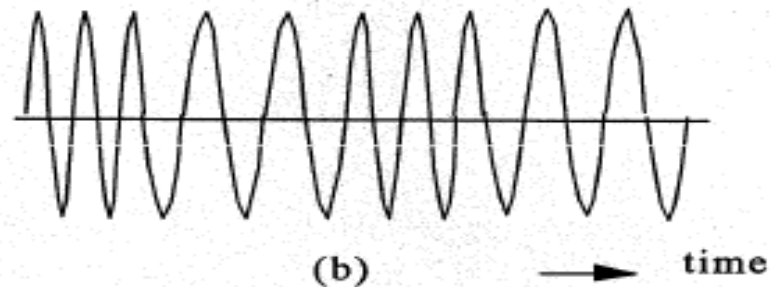
Example: Square Modulation

Square
modulating wave
 $m(t)$



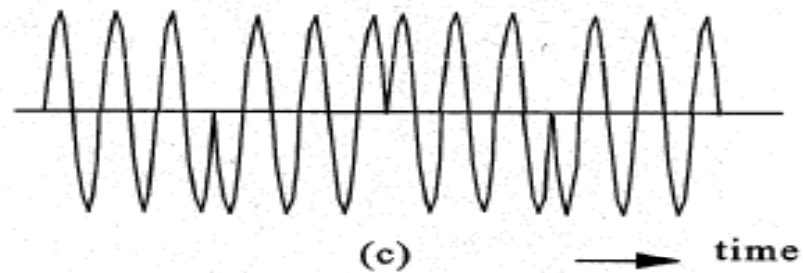
(a)

FM wave



(b)

PM wave



(c)

FM by a Sinusoidal Signal

- Consider a sinusoidal modulating wave

$$m(t) = A_m \cos(2\pi f_m t)$$

- Instantaneous frequency of resulting FM wave is

$$f_i(t) = f_c + k_f A_m \cos(2\pi f_m t) = f_c + \Delta f \cos(2\pi f_m t)$$

where $\Delta f = k_f A_m$ is called the **frequency deviation**, proportional to the amplitude of $m(t)$, and independent of f_m .

- Hence, the carrier phase is

$$\begin{aligned}\theta(t) &= 2\pi \int_0^t (f_i(\tau) - f_c) d\tau = \frac{\Delta f}{f_m} \sin(2\pi f_m t) \\ &= \beta \sin(2\pi f_m t)\end{aligned}$$

Where $\beta = \Delta f / f_m$ is called the **modulation index**

Example

□ Problem: a sinusoidal modulating wave of amplitude 5V and frequency 1kHz is applied to a frequency modulator. The frequency sensitivity is 40Hz/V. The carrier frequency is 100kHz. Calculate (a) the frequency deviation, and (b) the modulation index

□ Solution:

■ Frequency deviation $\Delta f = k_f A_m = 40 \times 5 = 200 \text{ Hz}$

■ Modulation index $\beta = \frac{\Delta f}{f_m} = \frac{200}{1000} = 0.2$

Spectrum Analysis of Sinusoidal FM Wave

- The FM wave for sinusoidal modulation is

$$\begin{aligned} s(t) &= A_c \cos[2\pi f_c t + \beta \sin(2\pi f_m t)] \\ &= A_c \underbrace{\cos[\beta \sin(2\pi f_m t)]}_{\text{In-phase component}} \cos(2\pi f_c t) - A_c \underbrace{\sin[\beta \sin(2\pi f_m t)]}_{\text{Quadrature-phase component}} \sin(2\pi f_c t) \end{aligned}$$

In-phase component

Quadrature-phase component

$$s_I(t) = A_c \cos[\beta \sin(2\pi f_m t)]$$

$$s_Q(t) = A_c \sin[\beta \sin(2\pi f_m t)]$$

- Hence, the **complex envelop** of FM wave is

$$\tilde{s}(t) = s_I(t) + js_Q(t) = A_c e^{j\beta \sin(2\pi f_m t)}$$

- $\tilde{s}(t)$ retains complete information about $s(t)$

$$s(t) = \text{Re}\left\{A_c e^{j[2\pi f_c t + \beta \sin(2\pi f_m t)]}\right\} = \text{Re}\left[\tilde{s}(t) e^{j2\pi f_c t}\right]$$

- $\tilde{s}(t)$ is periodic, can be expanded in Fourier series as

$$\tilde{s}(t) = \sum_{n=-\infty}^{\infty} c_n e^{j2\pi n f_m t}$$



$$\tilde{s}(t) = A_c e^{j\beta \sin(2\pi f_m t)}$$

where

$$\begin{aligned} c_n &= f_m \int_{-1/(2f_m)}^{1/(2f_m)} \tilde{s}(t) e^{-j2\pi n f_m t} dt \\ &= f_m A_c \int_{-1/(2f_m)}^{1/(2f_m)} e^{j[\beta \sin(2\pi f_m t) - 2\pi n f_m t]} dt \end{aligned}$$

- Let $x = 2\pi f_m t$

$$c_n = \frac{A_c}{2\pi} \int_{-\pi}^{\pi} \exp[j(\beta \sin x - nx)] dx$$

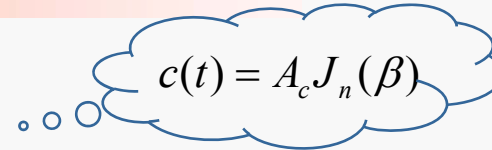
- n-th order **Bessel function** of the first kind $J_n(\beta)$ is defined as

$$J_n(\beta) = \frac{1}{2\pi} \int_{-\pi}^{\pi} \exp[j(\beta \sin x - nx)] dx$$

- Hence,

$$c_n = A_c J_n(\beta)$$

- Substituting c_n into $\tilde{s}(t)$


$$c(t) = A_c J_n(\beta)$$

$$\tilde{s}(t) = A_c \sum_{n=-\infty}^{\infty} J_n(\beta) \exp(j2\pi n f_m t)$$

- Hence, FM wave in **time domain** can be represented by

$$\begin{aligned} s(t) &= A_c \operatorname{Re} \left\{ \sum_{n=-\infty}^{\infty} J_n(\beta) \exp[j2\pi(f_c + n f_m)t] \right\} \\ &= A_c \sum_{n=-\infty}^{\infty} J_n(\beta) \cos[2\pi(f_c + n f_m)t] \end{aligned}$$

- In **frequency-domain**, we have

$$S(f) = \frac{A_c}{2} \sum_{n=-\infty}^{\infty} J_n(\beta) [\delta(f - f_c - n f_m) + \delta(f + f_c + n f_m)]$$

- Property 1: Narrowband FM (for small $\beta \leq 0.3$)

- Approximations

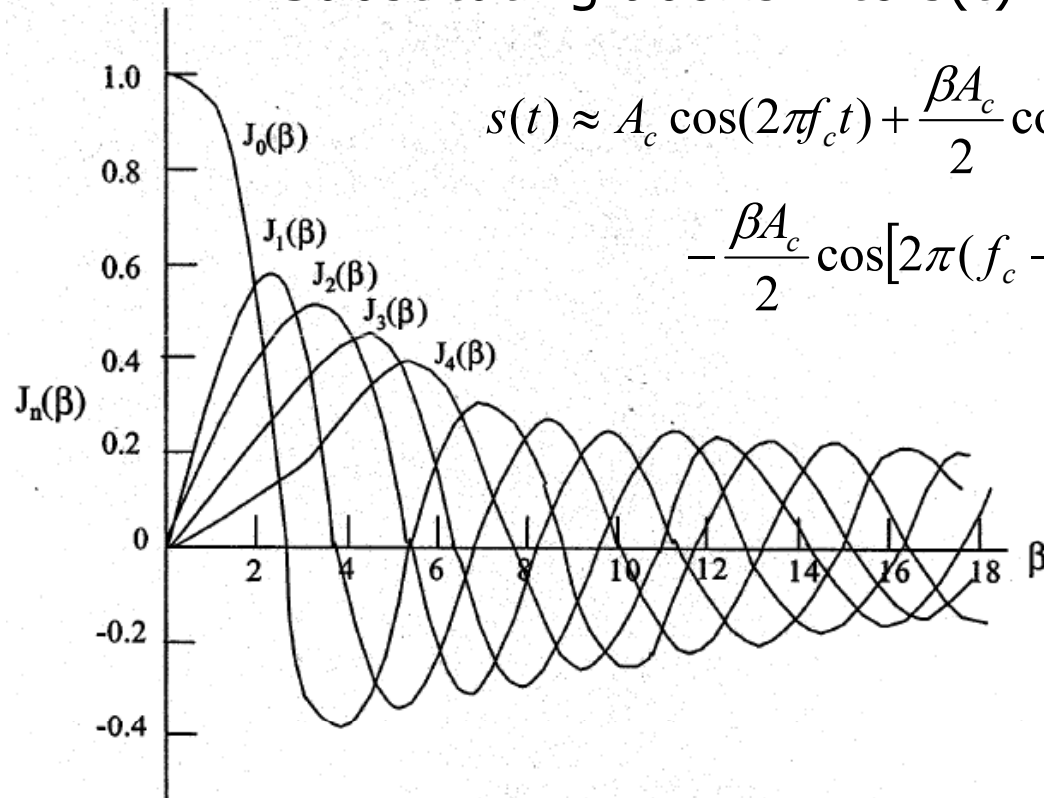
$$J_0(\beta) \approx 1$$

$$J_1(\beta) \approx \beta/2$$

$$J_n(\beta) \approx 0, n > 1$$

- Substituting above into $s(t)$

? In what ways do a conventional AM wave and a narrow band FM wave differ from each other



$$s(t) \approx A_c \cos(2\pi f_c t) + \frac{\beta A_c}{2} \cos[2\pi(f_c + f_m)t] - \frac{\beta A_c}{2} \cos[2\pi(f_c - f_m)t]$$

$$|J_n(\beta)| \rightarrow 0 \text{ as } \beta \rightarrow \infty$$

$$J_{-n}(\beta) = \begin{cases} J_n(\beta), & n \text{ even} \\ -J_n(\beta), & n \text{ odd} \end{cases}$$

Figure 8.4 - Plots of Bessel functions of the first kind.

Property 2: Wideband FM (for large $\beta > 1$)

- In theory, $s(t)$ contains a carrier and an infinite number of side-frequency components, with no approximations made

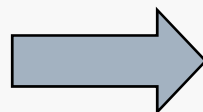
Property 3: Constant average power

- The envelop of FM wave is constant, so the average power is also constant, $P = A_c^2 / 2$

- The average power is also given by

$$s(t) = A_c \sum_{n=-\infty}^{\infty} J_n(\beta) \cos[2\pi(f_c + nf_m)t]$$

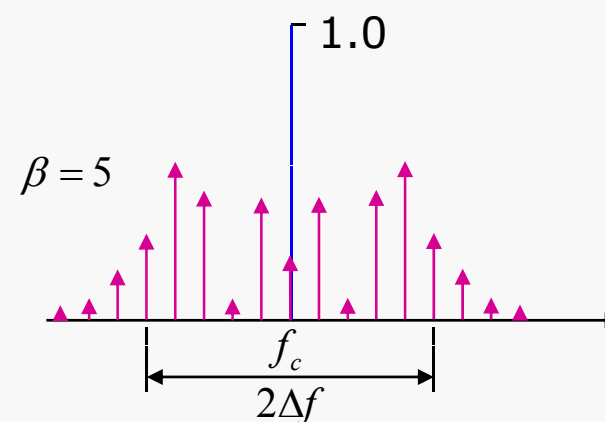
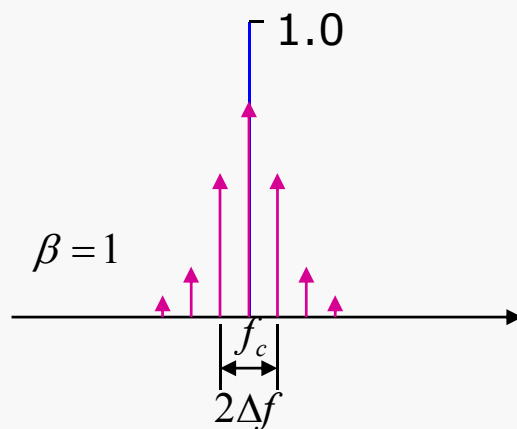
$$P = \frac{A_c^2}{2} \sum_n J_n^2(\beta) = \frac{A_c^2}{2}$$



$$\sum_{n=-\infty}^{\infty} J_n^2(\beta) = 1$$

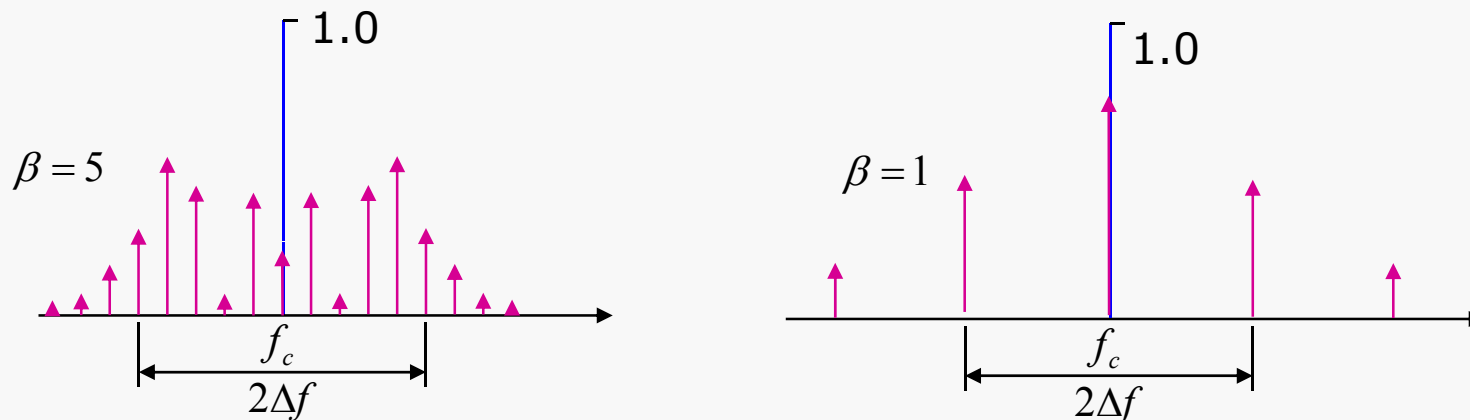
Example

- Goal: to investigate how the amplitude A_m , and frequency f_m , of a sinusoidal modulating wave affect the spectrum of FM wave
- Fixed f_m and varying $A_m \Rightarrow$ frequency deviation $\Delta f = k_f A_m$ and modulation index $\beta = \Delta f / f_m$ are varied



- Increasing A_m increases the number of harmonics in the bandwidth

- Fixed A_m and varying $f_m \Rightarrow \Delta f$ is fixed, but β is varied



- Increasing f_m decreases the number of harmonics but at the same time increases the spacing between the harmonics.

Effective Bandwidth of FM Waves

- Theoretically, FM bandwidth = infinite
- In practice, for a single tone FM wave, when β is large, B is only slightly greater than the total frequency excursion $2\Delta f$.
when β is small, the spectrum is effectively limited to
 $[f_c - f_m, f_c + f_m]$
- **Carson's Rule** approximation for single-tone modulating wave of frequency f_m

$$B \approx 2\Delta f + 2f_m = 2(1 + \beta)f_m$$

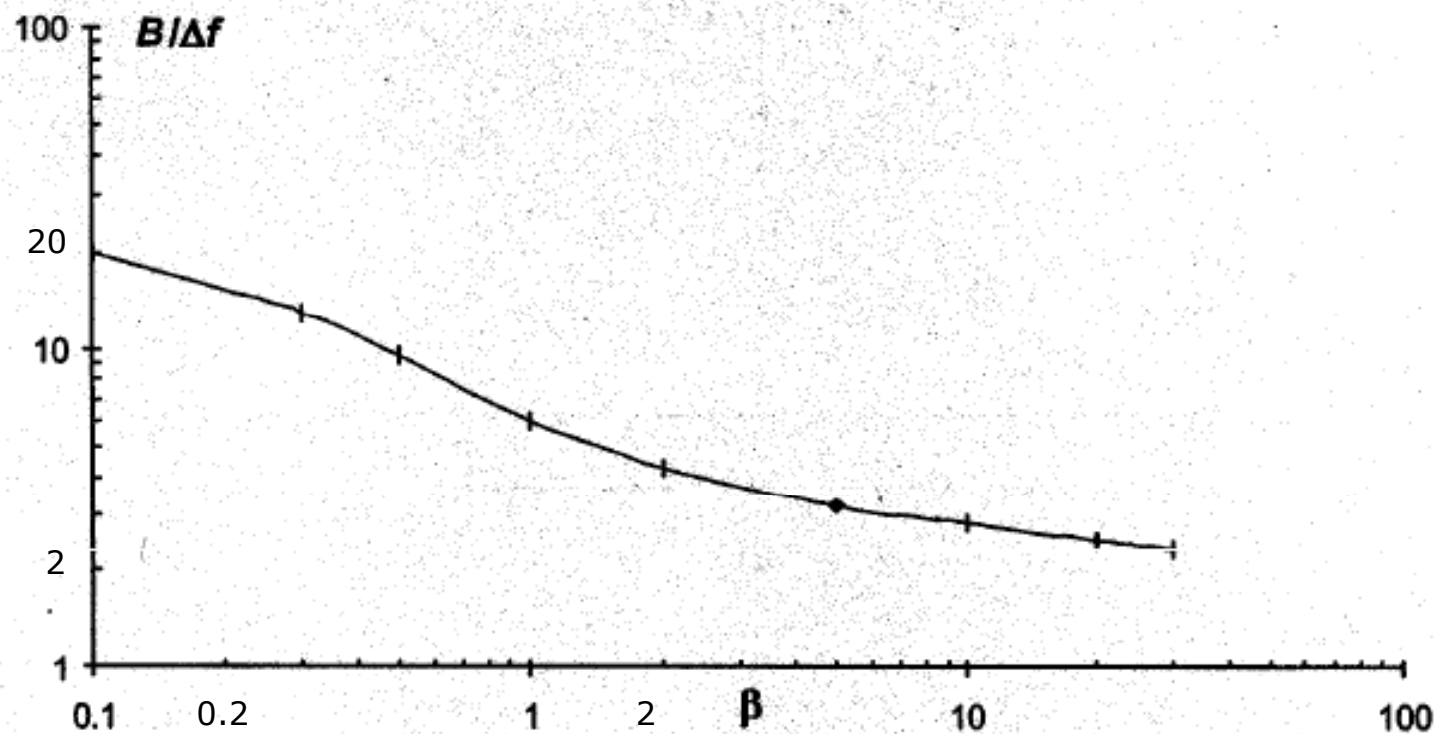
□ **99% bandwidth** approximation

- The separation between the two frequencies beyond which none of the side-frequencies is greater than 1% of the unmodulated carrier amplitude
- i.e $B \approx 2n_{\max}f_m$ where n_{\max} is the max n that satisfies

$$|J_n(\beta)| > 0.01$$

β	0.1	0.3	0.5	1.0	2.0	5.0	10	20	30
$2n_{\max}$	2	4	4	6	8	16	28	50	70

- A **universal curve** for evaluating the 99% bandwidth
 - As β increases, the bandwidth occupied by the significant side-frequencies drops toward that over which the carrier frequency



FM by an Arbitrary Message

- ❑ Consider an *arbitrary* $m(t)$ with highest freq component W
- ❑ Define **deviation ratio** $D = \Delta f / W$, where $\Delta f = k_f \max |m(t)|$
 $D \Leftrightarrow \beta$ and $W \Leftrightarrow f_m$
- ❑ Carson's rule applies as

$$B \approx 2\Delta f + 2W = 2W(1 + D)$$

- ❑ Carson's rule somewhat underestimate the FM bandwidth requirement, while universal curve yields a somewhat conservative result
- ❑ Assess FM bandwidth between the bounds given by Carson's rule and the universal curve

Example

- ❑ In north America, the maximum value of frequency deviation Δf is fixed at 75kHz for commercial FM broadcasting by ratio.
- ❑ If we take the modulation frequency $W = 15\text{kHz}$, which is typically the maximum audio frequency of interest in FM transmission, the corresponding value of the deviation ratio is $D = 75/15 = 5$
- ❑ Using *Carson's rule*, the approximate value of the transmission bandwidth of the FM wave is

$$B = 2 (75+15) = 180\text{kHz}$$

- ❑ Using *universal curve*,

$$B = 3.2 \Delta f = 3.2 \times 75 = 240\text{kHz}$$

Exercise

- Assuming that $m(t) = 10\text{sinc}(10^4 t)$, determine the transmission bandwidth of an FM modulated signal with $k_f = 4000$

Generation of FM waves

- ❑ Direct approach
 - Design an oscillator whose frequency changes with the input voltage => voltage-controlled oscillator (VCO)
- ❑ Indirect approach
 - First generate a narrowband FM signal first and then change it to a wideband single
 - Due to the similarity of conventional AM signals, the generation of a narrowband FM signal is straightforward.

Generation of Narrow-band FM

- Consider a **narrow band FM wave**

$$s_1(t) = A_1 \cos[2\pi f_1 t + \phi_1(t)]$$

where $\phi_1(t) = 2\pi k_1 \int_0^t m(\tau) d\tau$ $f_1 =$ carrier frequency
 $k_1 =$ frequency sensitivity

- Given $\phi_1(t) \ll 1$ with $\beta \leq 0.3$, we may use

$$\begin{cases} \cos[\phi_1(t)] \approx 1 \\ \sin[\phi_1(t)] \approx \phi_1(t) \end{cases}$$

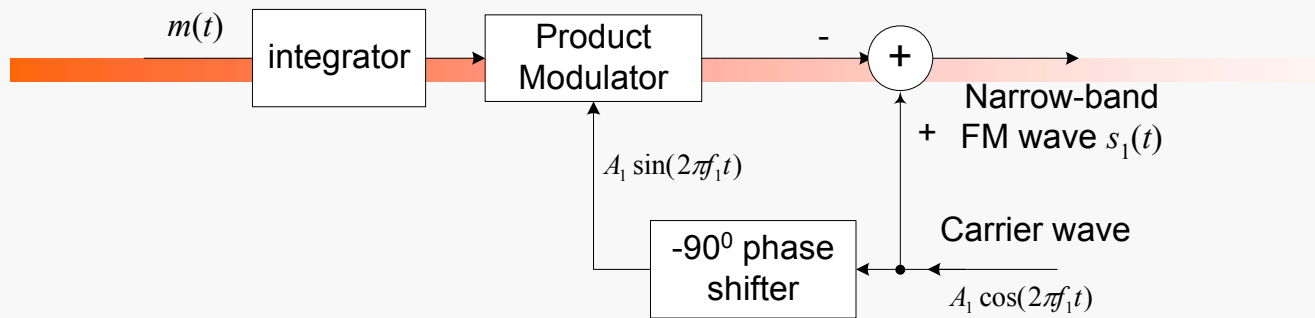
- Correspondingly, we may approximate $s_1(t)$ as

$$\begin{aligned} s_1(t) &= A_1 \cos(2\pi f_1 t) - A_1 \sin(2\pi f_1 t) \phi_1(t) \\ &= A_1 \cos(2\pi f_1 t) - 2\pi k_1 A_1 \sin(2\pi f_1 t) \int_0^t m(\tau) d\tau \end{aligned}$$

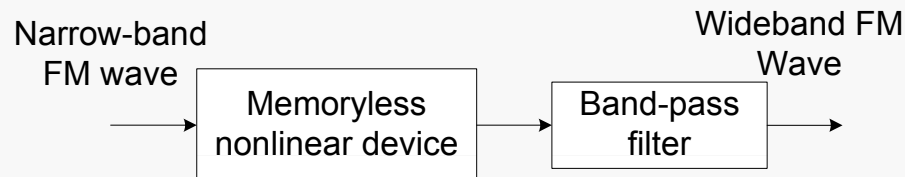
Narrow-band FM wave



- Narrow-band frequency modulator



- **Next**, pass $s_1(t)$ through a **frequency multiplier**, which consists of a non-linear device and a bandpass filter.



- The input-output relationship of the non-linear device is modeled as

$$s_2(t) = a_1 s_1(t) + a_2 s_1^2(t) + \dots + a_n s_1^n(t)$$

- The BPF is used to Pass the FM wave centred at nf_1 and with deviation $n\Delta f_1$ and suppress all other FM spectra

Example: frequency multiplier with $n = 2$

- Problem: Consider a square-law device based frequency multiplier

$$s_2(t) = a_1 s_1(t) + a_2 s_1^2(t)$$

with

$$s_1(t) = A_1 \cos\left(2\pi f_1 t + 2\pi k_1 \int_0^t m(\tau) d\tau\right)$$

- Specify the midband freq. and bandwidth of BPF used in the freq. multiplier for the resulting freq. deviation to be twice that at the input of the nonlinear device

- Solution:

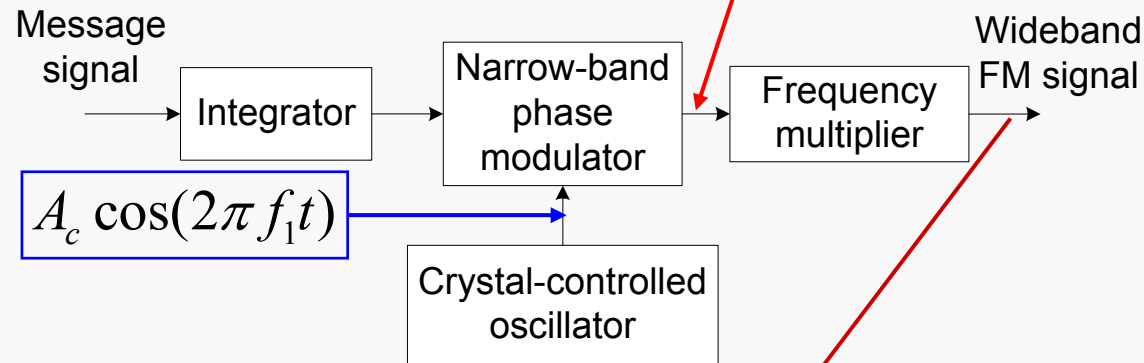
$$\begin{aligned} s_2(t) &= a_1 A_1 \cos\left(2\pi f_1 t + 2\pi k_1 \int_0^t m(\tau) d\tau\right) + a_2 A_1^2 \cos^2\left(2\pi f_1 t + 2\pi k_1 \int_0^t m(\tau) d\tau\right) \\ &= a_1 A_1 \cos\left(2\pi f_1 t + 2\pi k_1 \int_0^t m(\tau) d\tau\right) + \frac{a_2 A_1^2}{2} + \frac{a_2 A_1^2}{2} \cos\left(4\pi f_1 t + 4\pi k_1 \int_0^t m(\tau) d\tau\right) \end{aligned}$$

Removed by BPF with

$$\begin{aligned} f_c &= 2f_1 \\ \text{BW} &> 2\Delta f = 4\Delta f_1 \end{aligned}$$

- Thus, connecting the narrow-band frequency modulator and the frequency multiplier, we may build the wideband frequency modulator

$$s_1(t) = A_1 \cos\left(2\pi f_1 t + 2\pi k_1 \int_0^t m(\tau) d\tau\right)$$



$$s(t) = A_c \cos\left[2\pi f_c t + 2\pi k_f \int_0^t m(\tau) d\tau\right]$$

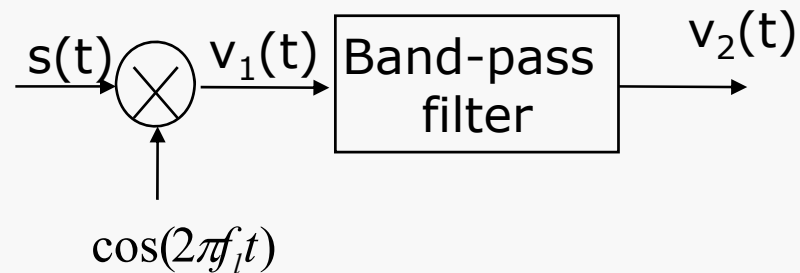
$$f_c = n f_1$$

$$k_f = n k_1$$

$$\Delta f = n \Delta f_1$$

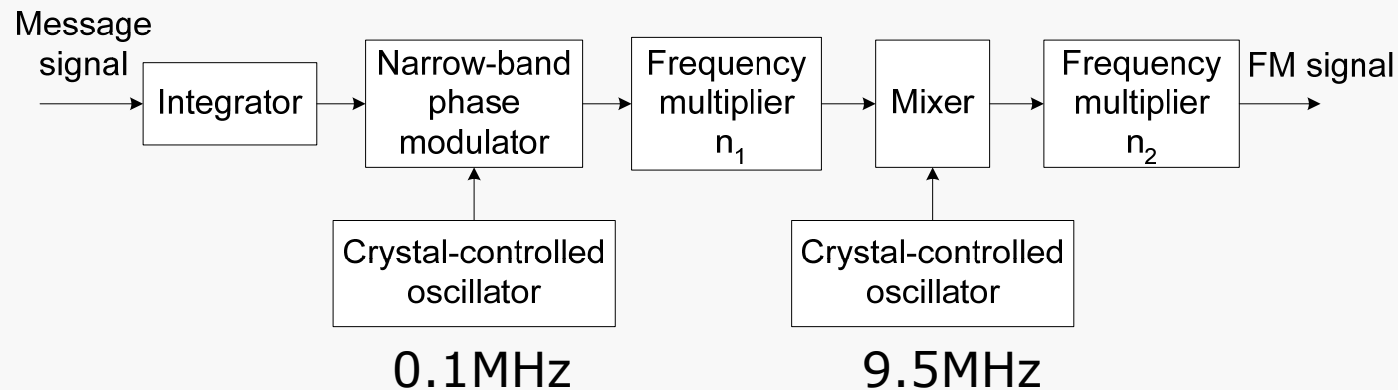
Mixer

- $f_c = nf_1$ may not be the desired carrier frequency. The modulator performs an up/down conversion to shift the modulated signal to the desired center freq.
- This consists of a mixer and a BPF



Exercise: A typical FM transmitter

- ❑ Problem: Given the simplified block diagram of a typical FM transmitter used to transmit audio signals containing frequencies in the range 100Hz to 15kHz.
- ❑ Desired FM wave: $f_c = 100\text{MHz}$, $\Delta f = 75\text{kHz}$.
- ❑ Set $\beta_1 = 0.2$ in the narrowband phase modulation to limit harmonic distortion.
- ❑ Specify the two-stage frequency multiplier factors n_1 and n_2



Demodulation of FM

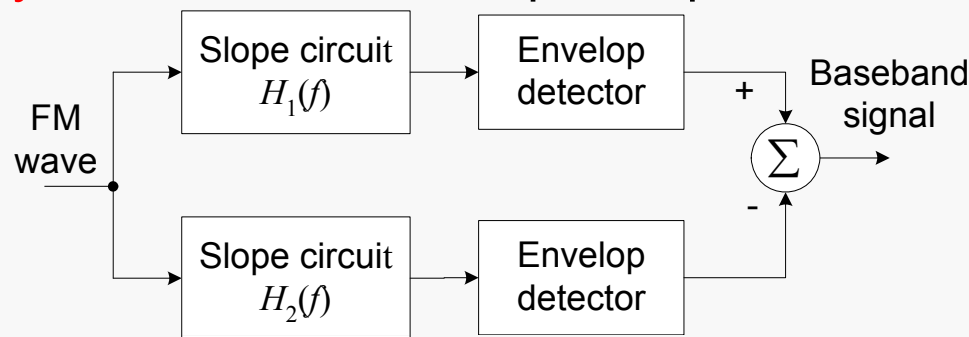
Balanced Frequency Discriminator

- Given FM wave $s(t) = A_c \cos\left(2\pi f_c t + 2\pi k_f \int_0^t m(\tau) d\tau\right)$

$$\frac{d}{dt}s(t) = -A_c \left[2\pi f_c t + 2\pi k_f m(t)\right] \sin\left[2\pi f_c t + 2\pi k_f \int_0^t m(\tau) d\tau\right]$$

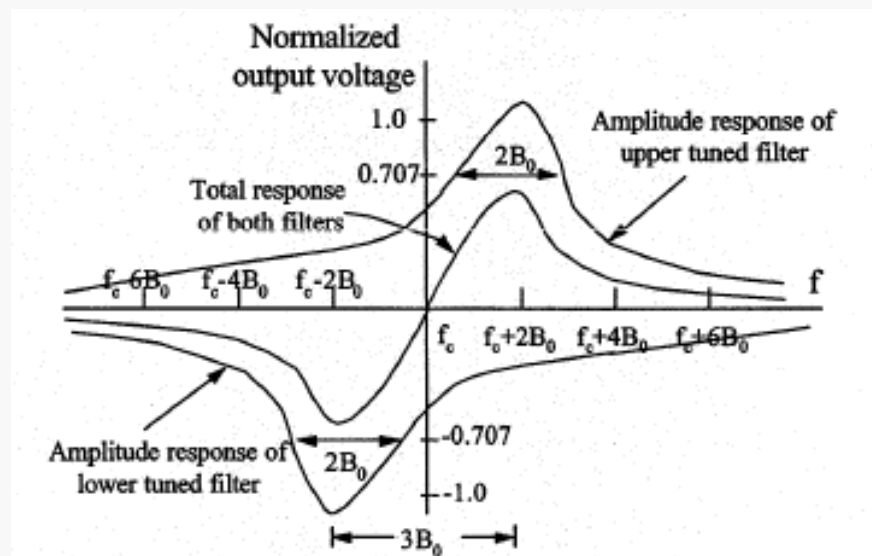
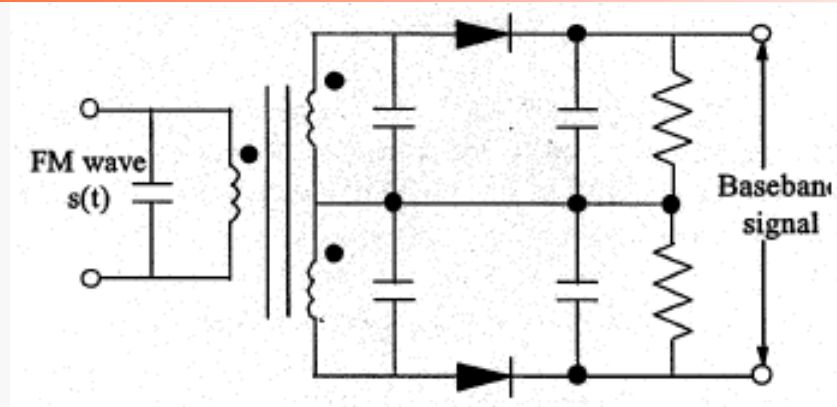
➔ Hybrid-modulated wave with AM and FM

- Differentiator + envelop detector = FM demodulator
- Frequency discriminator: a “freq to amplitude” transform device



$$H_1(f) = \begin{cases} j2\pi\alpha(f - f_c + B/2), & f_c - B/2 \leq f \leq f_c + B/2 \\ j2\pi\alpha(f + f_c - B/2), & -f_c - B/2 \leq f \leq -f_c + B/2 \\ 0, & \text{elsewhere} \end{cases} \quad H_2(f) = H_1(-f)$$

□ Circuit diagram and frequency response

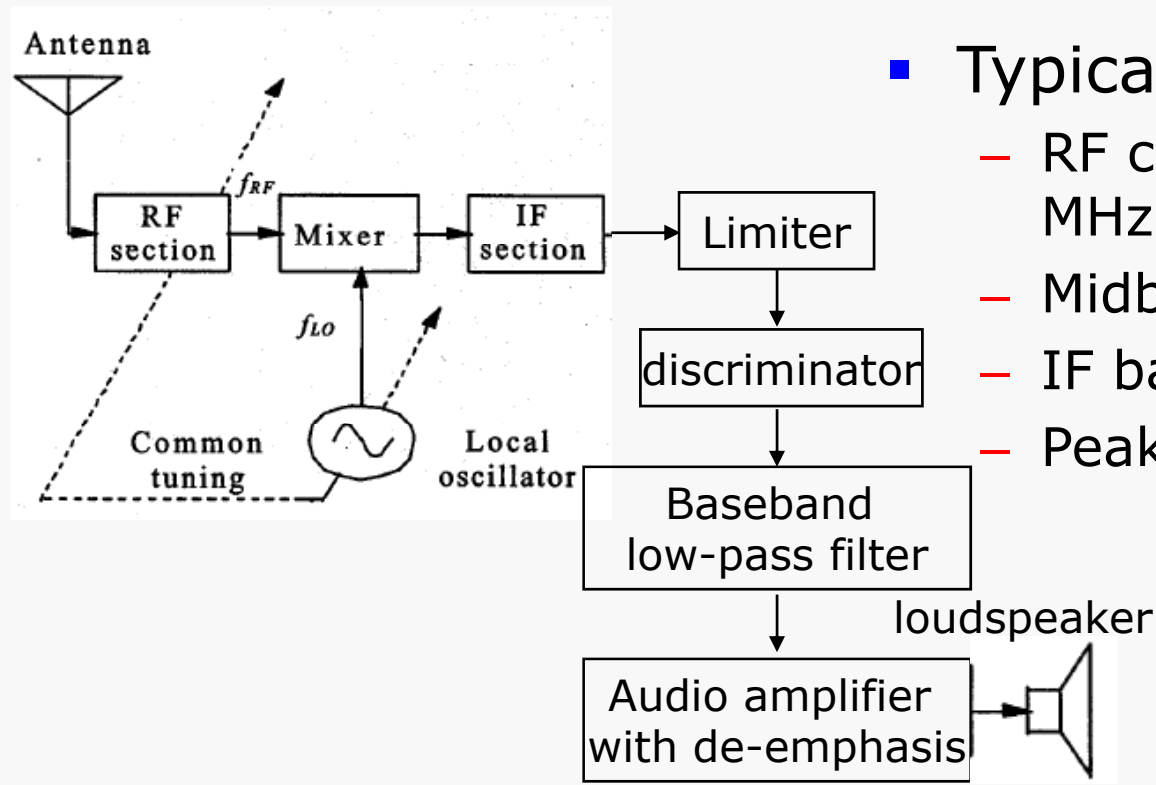


Think ...

- ❑ Compared with amplitude modulation, angle modulation requires a higher implementation complexity and a higher bandwidth occupancy.
- ❑ What is the usefulness of angle modulation systems?

Application: FM Radio broadcasting

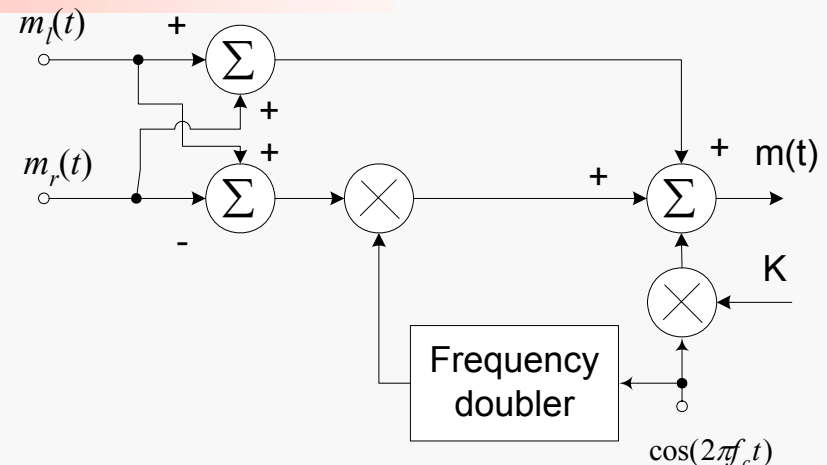
- ❑ As with standard AM radio, most FM radio receivers are of super-heterodyne type



- Typical freq parameters
 - RF carrier range = 88~108 MHz
 - Midband of IF = 10.7MHz
 - IF bandwidth = 200kHz
 - Peak freq. deviation = 75KHz

FM Radio Stereo Multiplexing

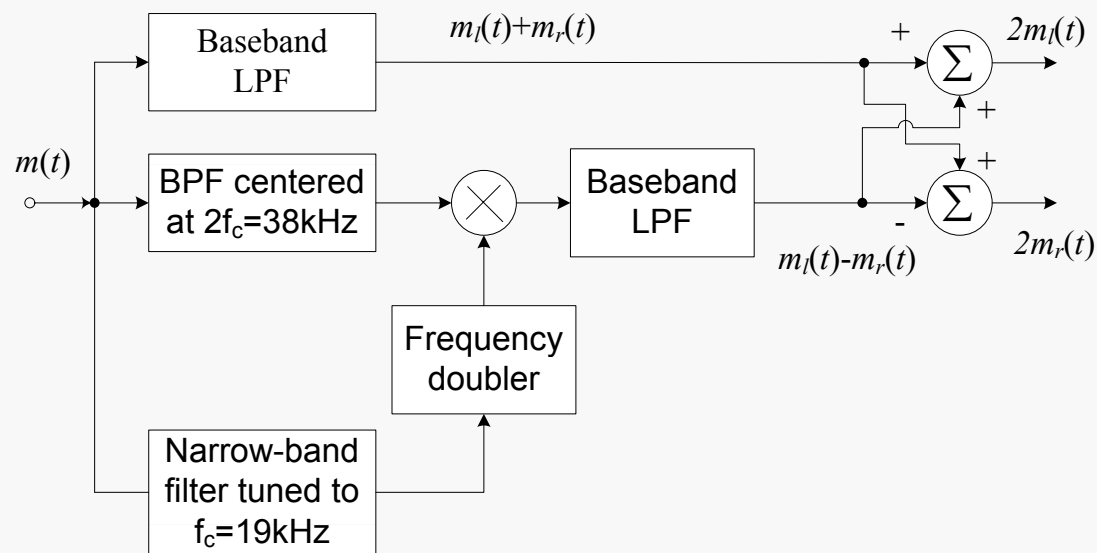
- ❑ **Stereo multiplexing** is a form of FDM designed to transmit two separate signals via the same carrier.
- ❑ Widely used in FM broadcasting to send two different elements of a program (e.g. **vocalist** and **accompanist** in an orchestra) so as to give a spatial dimension to its perception by a listener at the receiving end
 - The **sum signal** is left unprocessed in its baseband form
 - The **difference signal** and a 38-kHz subcarrier produce a DSBSC wave
 - The **19-kHz pilot** is included as a reference for coherent detection



$$m(t) = [m_l(t) + m_r(t)] + [m_l(t) - m_r(t)]\cos(4\pi f_c t) + K \cos(2\pi f_c t)$$

$$f_c = 19\text{kHz}$$

FM-Stereo Receiver



To two loudspeakers

Comparison of Analog-Modulation

□ Bandwidth efficiency

- SSB is the most bandwidth efficient, but cannot effectively transmit DC
- VSB is a good compromise
- PM/FM are the least favorable systems

□ Power efficiency

- FM provides high noise immunity
- Conventional AM is the least power efficient

□ Ease of implementation (transmitter and receiver)

- The simplest receiver structure is conventional AM
- FM receivers are also easy to implement
- DSB-SC and SSB-SC requires coherent detector and hence is much more complicated.

Applications

- ❑ SSB-SC:
 - Voice transmission over microwave and satellite links
- ❑ VSB-SC
 - Widely used in TV broadcasting
- ❑ FM
 - High-fidelity radio broadcasting
- ❑ Conventional AM
 - AM radio broadcasting
- ❑ DSB-SC
 - **Hardly used in analog signal transmission!**